Free Convection Flow and Heat Transfer of a Nano Fluid over a Porous Plate in a Darcy-Forccheimer Flow

Ramonu O.J¹, Alerechi L.W², Akinyemi T.O³

Abstract - A free convection flow and heat transfer of nanofluid over a porous plate in a Darcy-Forccheimer flow has been investigated. The governing partial differential equations are transformed into a system of ordinary differential equations using similarity transformation method and solved numerically using the Runge-Kutta fourth order alongside shooting technique. The influences of solutal Grashof number *Gm*, thermal Grashof number *Gr*, Brownian motion *Nb*, Lewis number Le and Thermophoresis *Nt* on the temperature, velocity and concentration distribution are investigated and the results are illustrated graphically. The reduced local Nusselt number and the reduced local Sherwood numbers are presented and compared with existing related studies; the comparisons are in excellent agreement.

Keywords: Darcy-Forccheimer, Free Convection, Heat Transfer, Nanofluid, Porous plate, Runge-Kutta, Grashof number.

1 INTRODUCTION

Nanofluid is an enhanced type of fluid made up of a two phase mixture prepared by dispersing nanometer sized materials in conventional or base fluids. The nanometer sized materials could be nanoparticles, nanowires, nanorods, nanotubes or nanofibers while the base fluids could be water, oils, biofluids, lubricants, organic liquid (refrigerants, glycols, ethylene or polymeric solutions) and common liquids. The combination of any of the above distinct materials and a base fluid yields a Nanofluid. Materials generally used as nanoparticles include metal oxides (e.g., alumina, silica, titania), oxide ceramics (e.g. Al₂O₃, CuO), chemically stable metals (e.g. gold, copper), carbon in various forms (e.g., diamond, graphite, carbon nanotubes, fullerene), metal carbides (e.g. SiC) and functionalized nanoparticles. Nanofluids are said to possess enhanced thermo physical properties such as thermal conductivity, thermal diffusivity, viscosity, and convective heat transfer coefficients compared to those of base fluids like oil or water. Wei and Huaqing[1].

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• Alerechi L.W completed his master degree program in Mechanical Engineering (Thermo-Fluid Option) in the University of Ibadan, Nigeria. He is a lecturer at Ignatius Ajuru University of Education, Port Harcourt, Rivers state. Nigeria. +2348036902675,

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• Akinyemi T.O. completed his master degree program in Mechanical Engineering (Thermo-Fluid Option) in the University of Ibadan, Nigeria. He is a lecturer at ESEP-LE BERGER Universite, Cotonou. +2347068364389, E-mail: engrtolu@gmail.com Choi [2] pioneered the proposition that fluids with nano particles suspended in them can be referred to as Nanofluids and concluded that they can be the next generation heat transfer fluids because they offer exciting new possibilities that can enhance heat transfer performance compared to pure liquids. Keblinski et al. [3] and Wang and Mujumdar[4] findings reveals that nanofluids can have significantly better heat transfer characteristics than the conventional fluids but this possibility is dependent upon the type, size and concentration of nanoparticles and the nanofluids transport through a porous media.

Xuan and Li [5] examined possible reasons for the improved effective thermal conductivity of nanofluids and highlighted four reasons which are the increased surface area due to suspended nanoparticles, the interaction and collision among particles, the intensified mixing fluctuation and turbulence of the fluid, and the dispersion of nanoparticles. Xuan and Roetzel [6] carried out a research which was the first to indicate a mechanism for heat transfer in nanofluids. They were able to propose thermal dispersion as a major mechanism of heat transfer in flowing fluid, as well as enhanced nanofluid thermal conductivity. However, no evidence was presented to support their conclusions.On the other hand, Eastman et al. [7] examined that with less than1% volume fraction of CuO, the convection heat transfer rate increased by more than 15% in water. Sun and Pop [8] examined the numerical solution of steady-state free convection heat transfer behaviour of nanofluids inside a triangular enclosure saturated by a porous media and they observed that the heat transfer rate

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increases with increased nanoparticle volume concentration at a low Rayleigh number, an opposite trend was discovered for a high Rayleigh number while Khan et al. [9] studied the free convection of nanofluids along a vertical plate in a porous media. In their own study, Servati et al. [10] numerically examined the forced convective MHD flow of a nanofluid in a channel partially filled with porous media. The steady mixed convection boundary layer flow of nanofluids past a vertical flat plate embedded in porous media was investigated by Ahmad and Pop [11] while Chamkha and Ismael [12] were able to conduct a numerical study to solve the problem of differentially heated and partially layered vertical porous cavity filled with a nanofluid on free convection, this was the first time such a numerical study was carried out and they applied the Darcy-Brinkman model. Falana and Ramonu [13], studied the effects of viscous dissipation and thermal radiation on an unsteady MHD boundary layer flow due to stretching sheet and heat transfer. Xuan and Li [14] found that heat transfer by forced convection is enhanced in nanofluids and concluded that much of this enhancement has to do with the type of nanoparticles used; cinvective studies were performed by them with oxide nanoparticles with results showing a moderately enhanced conductivity and increasing viscosity at the same time. The study concluded that the real advantage is expected in metallic nanofluids, which due to its high enhancement rate, require only a small volume fraction (<1%) that will keep viscosity almost unaffected but increase the heat transfer. Seddeek [15] studied mixed convection flow in view of Darcy-Forchheimer relation.

Pal and Mondal [16] examined hydromagnetic Darcy-Forchheimer flow of variable viscosity liquid while Sadiq and Hayat [17] investigated Darcy-Forchheimer flow of magneto Maxwell liquid bounded by a convectively heated sheet. Effects of internal heat generation, viscous dissipation and thermal radiation on an unsteady hydromagnetic flow past a stretching surface embedded in a porous medium was examined by Odunlami and Ramonu [18], the study concluded that there is a significant increase in the thermal boundary thickness and boundary layer temperature distribution with an increase in the radiation parameter. Umavathi et al. [19] performed numerical analysis of natural convective flow of nanofluids in a vertical rectangular duct using Darcy-Forchheimer-Brinkman model. Hayat et al. [20a] provided a comparative study for Darcy-Forchheimer flow of viscoelastic nanofluids and Recently Hayat et al. [20b] also discussed Darcy-Forchheimer flow of viscoelastic fluids with Cattaneo-Christov heat flux and homogeneousheterogeneous reactions. Ramonu and Odunlami investigated the combined influence of Brownian motion,

Thermophoresis and Lewis number on boundary layer flow of a nanofluid, they concluded that increase in the Thermophoresis parameter and Brownian motion parameter increases the temperature profile.

Nanofluids can be used to improve heat transfer and energy efficiency in a variety of thermal systems. This implies its great importance as a cooling fluid in many applications such as Engine cooling, Nuclear cooling system, Cooling of electronic circuit, Refrigeration, Enhancement of heat transfer exchange, Thermal storage, Biomedical application, Cooling of microchips, In defense and space application, Transportation, Petroleum industry, Inkjet printing, Environmental remediation, Surface coating, Fuel additives and Lubricant.

2 MATHEMATICAL ANALYSIS

Here, consideration is given to a steady, laminar, incompressible and two dimensional boundary layer free convection flow and heat transfer of a nanofluid over a porous plate embedded in a porous medium. The x-axis is taking along the surface of the porous plate and the y-axis perpendicular to it. The temperature Tw and concentration Cw on the surface of the plate are kept constant, and assumed to be greater than the ambient temperature and concentration, $T \propto$ and $C \infty$, respectively.

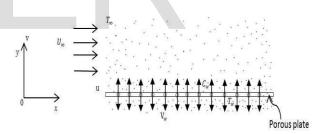


Fig. 1. Geometry of the physical model

The governing equations for the conservation of mass, momentum which is based on the Darcy-Forchheimer model, thermal energy and nanoparticle concentration are expressed as follow:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \tag{1}$$

$$\begin{aligned} & u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = v\frac{\partial^2 u}{\partial y^2} - \frac{v}{\kappa}(u - u_{\infty}) - \frac{K^*}{\sqrt{K}}(u^2 - u_{\infty}^2) + g\beta (T - T_{\infty}) + g\beta^* (C - C_{\infty}) \end{aligned}$$
(2)

$$\mathbf{u}_{\partial x}^{\partial T} + \mathbf{v}_{\partial y}^{\partial T} = \alpha_{\partial y^2}^{\partial^2 T} + \tau \left[D_B \frac{\partial C}{\partial y} \left(\frac{\partial T}{\partial y} \right) + \frac{D_T}{T_{\infty}} \left(\frac{\partial T}{\partial y} \right)^2 \right]$$
(3)

$$\mathbf{u}\frac{\partial C}{\partial x} + \mathbf{v}\frac{\partial C}{\partial y} = \mathbf{D}_{\mathrm{B}}\left(\frac{\partial^{2} C}{\partial y^{2}}\right) + \frac{D_{T}}{T_{\infty}}\left(\frac{\partial^{2} T}{\partial y^{2}}\right)$$
(4)

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Where u and v are the velocity components in the x and y directions respectively, $u \infty$ is the free stream velocity, μ is the viscosity, T is the temperature of the nanofluid, C is the concentration of the nanofluid, Tw is the temperature along the porous plate, Cw is the concentration along the porous plate, $T\infty$ and $C\infty$ are the ambient temperature and concentration respectively, $v = \frac{\mu}{\varrho}$ is the kinematic viscosity, Gm is the solutal Grashof number, Gr is the thermal Grashof number, $\kappa = k_0 x$ is the Darcy permeability of the porous medium, D_B is the Brownian motion coefficient, D_T is the thermophoresis coefficient, k is the thermal conductivity, $(\rho c)p$ is the heat capacitance of the nanoparticles, $(\rho c)f$ is the heat capacitance of the base fluid, $\alpha = \frac{k}{(qc)f}$ is the thermal diffusivity, $\tau = \frac{(qc)p}{(qc)f}$ is the ratio between the heat capacitance of the nanoparticles and the heat capacitance of the base fluid.

With the associated boundary conditions:

At
$$y = 0$$

 $u = 0$; $v = 0$; $T = T_w$; $C = C_w$
(5)
At $y \to \infty$
 $u \to u_\infty$; $T \to T_\infty$; $C \to C_\infty$
(6)

Further, we seek for a similarity solution of Equations (1) to (4) subject to the boundary conditions (5) and (6). The governing partial differential forms can be solved by converting them to ordinary differential equations; this is done by using similarity functions:

$$\begin{split} \Psi(x,y) &= \sqrt{u_{\infty}vx}f(\eta) \\ and \\ \eta &= {y/x (Re_x)^{\frac{1}{2}}} = y(\frac{u_{\infty}}{vx})^{\frac{1}{2}} \\ \theta(\eta) &= \left(\frac{T-T_{\infty}}{T_w-T_{\infty}}\right) \quad \varphi(\eta) = \left(\frac{C-C_{\infty}}{C_w-C_{\infty}}\right) \end{split}$$
(7)

where the free stream function $\Psi(x, y)$ defined by;

$$U = \frac{d\Psi}{dy} \quad ; V = -\frac{d\Psi}{dx} \tag{8}$$

Applying these similarity variables on the governing partial differential equations, transformed conservation equations and boundary conditions are then obtained as follows

$$f^{'''} + \frac{1}{2} f f^{''} - K_1 (f^{'} - 1) - K_2 [(f^{'})^2 - 1] + Gr_x \theta + Gm_x \phi = 0$$
(9)

$$\frac{\theta''}{Pr} + Nb\varphi'\theta' + Nt(\theta')^2 + \frac{1}{2}f\theta' = 0$$
(10)

$$\phi'' + \frac{Nt}{Nb}\theta'' + \frac{Le}{2}f\phi' = 0$$
(11)

The boundary conditions:

$$\eta = 0, f'(0) = 0, f(0) = 0, \theta(0) = 1, \phi(0) = 1$$
 (12)

At
$$y \to \infty$$

 $\eta \to \infty, f'(\infty) \to 1, \theta(\infty) \to 0, \phi(\infty) \to 0$ (13)

However, the quantities of physical and engineering interest are the skin friction coefficient, reduced Nusselt number and reduced Sherwood number:

Having the knowledge of the velocity field, the skin-friction at the plate is obtained in a non-dimensional form and given by

$$C_f \operatorname{R} e_x^{\frac{1}{2}} = f''(0),$$

Also, with the knowledge of the temperature field, the rate of heat transfer coefficient can be obtained, which is in a non-dimensional form, in terms of the Nusselt number, and given by

$$Nu_x = -\operatorname{R} e_x^{\frac{1}{2}} \theta'(0),$$

Having the knowledge of the concentration field, the rate of mass transfer coefficient can be obtained, which is in a nondimensional form, in terms of the Sherwood number, is given by

 $Sh_x = -\operatorname{R} e_x^{\frac{1}{2}} \phi'(0).$

3 NUMERICAL METHOD FOR SOLUTION

The set of coupled non-linear governing boundary layer equations together with boundary conditions are solved numerically by using Runge-Kutta fourth order technique along with shooting method. The higher order non-linear differential equations are converted into first order simultaneous linear differential equations which are further transformed into initial value problem by applying the shooting technique and the resultant initial value problem is solved by employing Runge-Kutta fourth order method. $f = y_1$, $f' = y_2$, $f'' = y_3$,

$$\theta = y_4, \qquad \theta' = y_5, \varphi = y_6, \varphi' = y_7$$

 $f' = y'_1 = y_2,$
 $f'' = y'_2, = y_3$
 $f'' ' = y'_3$ and
 $\theta' = y'_4 = y_5, \varphi' = y'_6 = y_7$

4. RESULTS AND DISCUSSION

The transformed non linear equations (9)-(11) subjected to the boundary conditions (12) and (13) was solved numerically using the Runge Kutta fourth order algorithm which is implemented in MATLAB as an m-file in the form of ode with f "(0) and $\theta'(0)$ chosen a prior until the boundary conditions at infinity are satisfied. Resulting from the numerical calculations, the temperature profile, velocity profile and the nanoparticle concentration distribution for the fluid flow being considered are obtained with their behaviours discussed for varying governing parameters of interest which are solutal Grashof number Gm, thermal Grashof number Gr, Thermophoresis parameter N_t , Brownian motion N_b , permeability parameter K_1 , Lewis number Le, and Prandtl number Pr. Table 1: shows the numerical values of reduced Nusselt number Nu and reduced Sherwood number Sh for various values of Nt and *Nb* to validate the present study with existing literatures by Khan and Pop [21], Makinde and Aziz [22] The comparison is found to be in excellent agreement.

Table 1: Comparisons of results for reduced Nusselt number $-\theta'(0)$ and reduced Sherwood number $-\phi'(0)$ with *Le*=*Pr*=10, *K*₁= *K*₂= 0

Nb	Nt	Makinde		Khan	and	Present	
		andAziz [22]		Pop [21]		Study	
		$-\theta'(0)$	<i>−φ′</i> (0	$-\theta'(0)$	<i>−</i> ¢ ′(0	$-\theta'(0)$	<i>−</i> ¢ ′(0
0.1	0.1	0.9524	2.1294	0.9524	2.1294	0.9523	2.1294
0.2	0.1	0.5056	2.3819	0.5056	2.3819	0.5055	2.3819
0.3	0.1	0.2522	2.4100	0.2522	2.4100	0.2522	2.4100
0.4	0.1	0.1194	2.3997	0.1194	2.3997	0.1194	2.3997
0.5	0.1	0.0543	2.3836	0.0543	2.3836	0.0543	2.3836

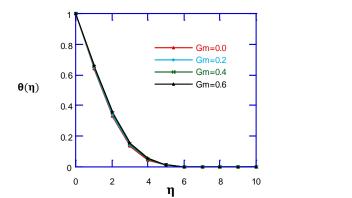


Fig. 2 Temperature Profile for various values of G_m when Nt=Nb=Nt/Nb=0.1, K_1 =0.1and K_2 =0.1,Le=0.5,Gr=0.5,Pr=0.7

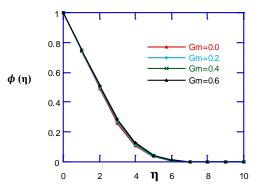


Fig.3 Concentration distribution for various values of G_m when Nt=Nb=Nt/Nb=0.1, K_1 =0.1and K_2 =0.1,Le=0.5,Gr=0.5,Pr= 0.7

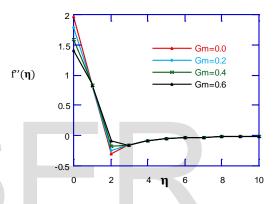


Fig.4 Skin friction for various values of G_m when Nt=Nb=Nt/Nb=0.1, K_1 =0.1and K_2 =0.1,Le=0.5,Gr=0.5,Pr=0.7

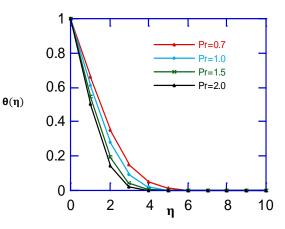


Fig. 5 Temperature Profile for various values of Pr when Nt=Nb=Nt/Nb= $0.1, K_1=0.1$ and $K_2=0.1$, Le= $0.5, Gr=0.5, G_m=0.5$

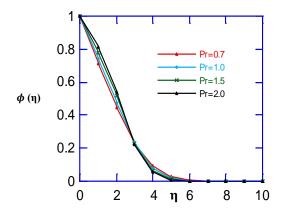


Fig.6 Concentration distribution for various values of Pr when Nt=Nb=Nt/Nb=0.1, K_1 =0.1and K_2 =0.1,Le=0.5,Gm=0.5, G_r =0

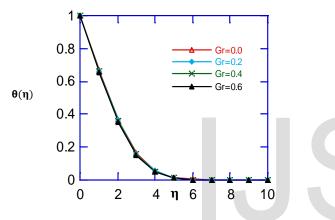


Fig.7 Temperature Profile for various values of G_r when Nt=Nb=Nt/Nb=0.1, K_1 =0.1and K_2 =0.1,Le=0.5,Gm=0.5,Pr=0.7

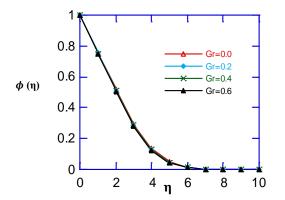


Fig.8 Concentration distribution for various values of G_r when Nt=Nb=Nt/Nb=0.1, K_1 =0.1and K_2 =0.1,Le=0.5,Gm=0.5,Pr=0.7

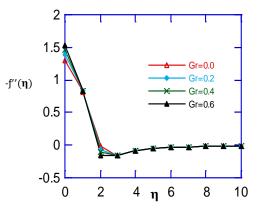


Fig.9 Skin friction for various values of *G_r* when Nt=Nb=Nt/Nb=0.1,*K*₁=0.1and*K*₂=0.1,Le=0.5,Gm=0.5,Pr=0.7

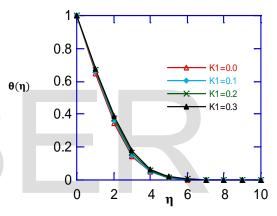


Fig.10 Temperature Profile for various values of K_1 when Nt=Nb=Nt/Nb=0.1, $G_r = 0.5$ and $K_2=0.1$, Le=0.5, $G_m=0.5$, Pr=0.7

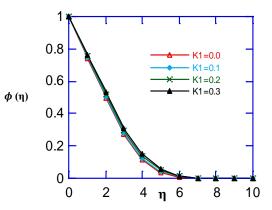


Fig.11 Concentration distribution for various values of K_1 whenNt=Nb=Nt/Nb=0.1, G_r =0.5and K_2 =0.1,Le=0.5, G_m =0.5,Pr=0.7

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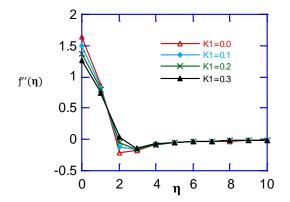


Fig.12 Skin friction for various values of K_1 when Nt=Nb=Nt/Nb=0.1, G_r =0.5and K_2 =0.1,Le=0.5, G_m =0.5,Pr=0.7

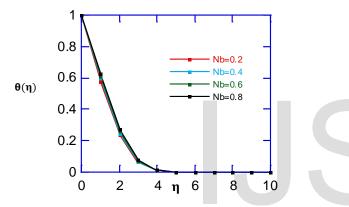


Fig.13 Temperature profile for various values of N_b when Nt=Nt/Nb=0.1, $G_r = 0.5, K_1 = 0.1$, $K_2=0.1$, Le=0.5, $G_m=0.5$, Pr=0.7

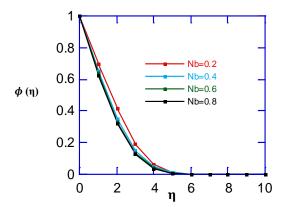


Fig.14 Concentration distribution for various values of N_b when Nt=Nt/Nb=0.1, $G_r = 0.5, K_1 = 0.1$, $K_2 = 0.1, Le=0.5, G_m = 0.5, Pr=0.7$

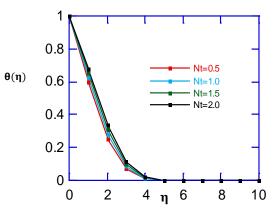


Fig.15 Temperature profile for various values of N_t when Nb=Nt/Nb=0.1, $G_r = 0.5, K_1 = 0.1$, $K_2=0.1$, Le=0.5, $G_m=0.5$, Pr=0.7

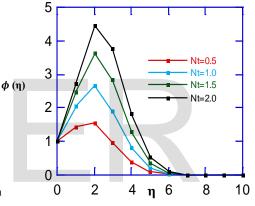


Fig.16 Concentration distribution for various values of N_t when Nb=Nt/Nb=0.1, $G_r = 0.5, K_1 = 0.1$, $K_2=0.1$, Le=0.5, $G_m=0.5$, Pr=0.7

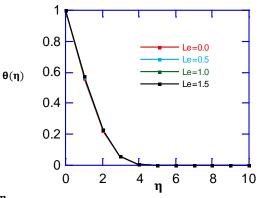


Fig.17 Temperature profile for various values of Le when Nb= $N_t = Nt/Nb=0.1$, $G_r = 0.5$, $K_1 = 0.1$, $K_2 = 0.1$, $G_m = 0.5$, Pr=0.7

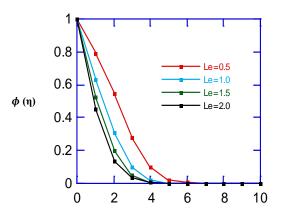


Fig.18 Concentration distribution for various values of when Le Nb= $N_t = Nt/Nb=0.1$, $G_r = 0.5$, $K_1 = 0.1$, $K_2=0.1$, $G_m=0.5$, Pr=0.7

Fig.2 indicates that an increase in solutal Grashof number Gm result to an increase in the temperature profile while fig.3 also illustrates that increasing solutal Grashof number Gm, increases the concentration distribution. It is observed in Fig.4 that the skin friction increases with solutal Grashof number Gm. Fig.5 shows the influence of the Prandtl number Pr on the nanofluid temperature distribution. It indicates that the temperature distribution decreases with an increase in Prandtl number Pr; since a large Prandtl number, implies a small thermal diffusivity which in turn reduces the thermal boundary layer thickness while fig.6 illustrates an increases.

Likewise, the effects of thermal Grashof number Gr on the temperature profile, concentration distribution and skin friction are illustrated in fig.7 to fig.9 respectively; it is observed that increasing the thermal Grashof number Gr increases the temperature profile, concentration distribution and skin friction.

It observed in fig.10 that as the permeability parameter K_1 increases, the temperature profile decreases while fig.11 also indicates that increasing permeability parameter K_1 decreases the nanofluid concentration distribution. Fig.12 illustrates the influence of permeability parameter K_1 on skin friction; it is observed that the skin friction increases with increasing permeability parameter K_1 .

It is illustrated in fig.13 that as the Brownian motion parameter N_b increases, the temperature gradient magnitude at the wall decreases. This implies that an increase in Brownian motion parameter N_b increases the temperature profile while fig.14 illustrates a decrease in the concentration distribution as Brownian motion parameter N_b increases.

Fig.15 indicates that increasing the Thermophoresis parameter N_t result to an increase in the boundary layer thickness and in turn increases the temperature profile while fig.16 also illustrate an increase in the concentration boundary layer thickness with an increase in Thermophoresis parameter N_t .

Fig.17 shows that increasing the Lewis number Le results in a small decrease in the temperature profile while fig.18 also indicates a decrease in concentration distribution as the Lewis number Le increases, which is as a result of a smaller molecular diffusivity as the Lewis number Le increase and in turn decreases the concentration distribution.

5. CONCLUSION

This study has numerically analyzed free convection flow and heat transfer of a nanofluid over a porous plate in a Darcy-Forchheimer flow. Applying the similarity transformation method, the governing partial differential equations are transformed into non-linear ordinary differential equations and the resulting equation is solved using Runge-Kutta fourth order method alongside shooting method. The effects of the governing parameters on the flow have been investigated. The following conclusions are drawn from the analysis:

- 1. It is observed that increasing the thermal Grashof number *Gr* and the solutal Grashof number *Gm* increase the temperature profile, concentration distribution and the skin friction.
- 2. The result indicates that as the permeability parameter K_1 increases, the temperature profile decreases while the skin friction increases
- 3. The temperature profile increases with the Brownian motion parameter N_b and the Thermophoresis parameter

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